

## STATE OF THE ART OF MICRO-CUTTING

Optimizing each processing process requires a clear knowledge of the mechanisms by which it takes place. In the case of steel processing by cutting, in the middle of the 1940s, a clear model was established according to which the process of chip formation takes place [1, 2]. Based on this model, it was later possible to optimize machining [3-7], with the aim of more efficient steel machining in terms of time spent, better machined surface quality and increased tool life. The established chip formation mechanism is valid only in the case when processing homogeneous materials, materials that are not brittle in nature and where the value of cutting depth is significantly higher than the value of the tool radius, thus its influence on the machining process can be neglected.

When it comes to micro-cutting, there are two approaches by which it is defined [8]:

First approach:

- micro-cutting is a set of all operations that are performed on components of micro/meso dimensions and products in the range of 100  $\mu\text{m}$  up to 10 mm;
- micro-cutting characterizes the requirements for the production of high-precision products, complex geometric shapes from a wide range of materials in a defined range of measures;
- micro-cutting involves the use of special tools (micro tools with a diameter of 50  $\div$  500  $\mu\text{m}$ ), small chip thickness (submicron to several micrometers) and speed (50k  $\div$  200k  $\text{min}^{-1}$ ).

As a consequence, the main difference between micro and macro-cutting is the dominance of sliding and scratching over shear and the need to take micro-structural effects into account.

Second approach:

The definition of micro-cutting from the point of view of chip thickness dimensions can be classified into:

- Macro: machining in conventional modes where the thickness of the chip is an order of magnitude greater than the tool tip radius and the process is dominated by shear. In doing so, the micro-structural effects can be neglected. The value of chip thickness is above 10  $\mu\text{m}$ ;
- Micro/meso: this processing is characterized by the dominance of scratching, friction, elastic and plastic deformation with the conclusion that the tool tip radius is approximately equal to the thickness of the chip. The thickness of the chip ranges from sub micro to several micrometers;
- Nano: this term is usually associated with ultra-precision machining with diamond tools that have the ability to sharpen without a radius or with a small tip radius so that the thickness of the chip can be in the nanometer range.

Industries such as automotive, special purpose, food and others, not infrequently need to introduce newer, more modern materials during product design, and later their production from them. Materials such as various types of glass, ceramics or stone-based materials are on the list of materials often used in the mentioned industries. They have found application from MEMS systems to various types of lenses, and even moving elements that must have good thermal properties and wear resistance. These materials, which are brittle in nature, are classified as very desirable, thanks to their high hardness and good thermal characteristics. However, the introduction of materials of this type in various industries, regardless of all its positive characteristics, has its downsides, which are the difficult machinability of these materials, as well as insufficient knowledge of the mechanisms by which it takes place.

Due to its hardness, the processing of brittle materials takes place at much smaller depths compared to materials that have more pronounced plastic properties. By reducing the cutting depth to one millimeter or less, the machining process shifts from the macro domain to the micro-cutting domain. When it comes to micro-cutting, it can be said that the set cutting mechanisms are no longer valid. Among the main causes are some of the factors such as: pronounced brittleness of the material being processed, rounding of the tool tip whose radius in this case is greater than the depth of cut and inhomogeneity (heterogeneity) of the material being processed. The mechanism of micro-cutting of brittle materials, which by its nature clearly defines the process of chip formation and the conditions under which it takes place, is still not clearly and precisely defined.

What is additionally interesting is that although the mentioned types of materials are brittle in nature, they can be processed in the so-called plastic deformation regime (ductile mode), where the processing is performed without the presence of destruction [9-13]. In the ductile mode, no separation of the material is noticed, but the complete processing takes place thanks to the return elastic and plastic deformations. This type of processing is desirable because it does not require post-treatment to ensure a smooth, transparent surface, or even to remove residual cracks that occur during the cutting process, which could jeopardize the integrity of the structure itself.

Not so long ago, more complex research in the field of micro-cutting was started. All this research is conducted in three basic directions:

- identification of the indentation process under static and dynamic force and the micro-cutting process;
- examination of the influence of the kinematics of the micro-cutting process on the machinability of brittle materials;
- examination of the influence of tool geometry on the micro-cutting process.

### ***Identification of the indentation process under static and dynamic force and the micro-cutting process***

In order to clarify the phenomena that occur during the micro-cutting process, the researchers conducted indentation experiments under static and dynamic indentation force, and the micro-cutting (scratching) process with an appropriate cutting tool. The main goal of these experiments was to: explain the mechanism of chip formation, to reach the value of the critical depth of tool penetration, to determine the values of force intensity and specific energy of micro-cutting as a function of tool geometry, speed and depth of micro-cutting.

Unlike materials with pronounced plasticity, where during micro cutting the material is separated in the form of extrusion [14-24], in brittle materials this process takes place by the mechanism of brittle destruction. The process of brittle destruction takes place through the phenomenon of cracking in the cutting zone, then the separation of parts of the material, accompanied by the appearance of crushing of the material. Research aimed at examining the shape and manner of crack formation within the material dates back to the mid-1970s [25-29]. Cracks that form in the cutting zone can be classified into three basic forms:

- medial cracks,
- lateral cracks,
- radial cracks.

Prediction of the intensity of material destruction, i.e., crack growth during the micro-cutting process is necessary for the formation of a valid micro-cutting mechanism. Residual cracks and their unwanted growth within the material can lead to significant side effects. Their presence within the material after the processing process can affect the integrity of the structure, while their uncontrolled growth can lead to undesirable quality of the machined surface. One of the methods for predicting crack length was presented by B.R. Lawn and M.V. Swain [30]. Their research was based on the indentation of indenter under static force. By processing the experimental results using the "Boussinesq" method, they found that there is a proportionality between the values of the indentation force and the crack length that occur within the material during and after the indentation process.

Further research B.R. Lawn conducted with his associates [28, 29, 31-33], found that the residual stresses present within the material after the completion of the indentation process are responsible for the further growth of the medial cracks and after the unloading of the material. One of the causes of residual stresses is the heterogeneity of the material being processed. More precisely, the different hardness of the minerals of which the material is composed can be the initiator for residual stresses. The same conclusions were reached in research [34, 35].

A. Chandra et al [36] presented their model for predicting material destruction. Experimental analysis confirmed the great matching of the model with the obtained values. However, what must be singled out, and what has been established by their research, is that the growth of lateral cracks occurs during the unloading of the material. On the other hand, B.R. Lawn and A.G. Evans [27] presented a model for predicting the growth of medial/radial cracks that provides a functional relationship between the size of the critical value of the crack and the indentation force, necessary for the continuation of further crack growth.

In addition to the method of indentation under static force, in previous research, the method of scratching was also used. The main difference between this method and the indentation is that due to the interaction of the tool and the workpiece, both the normal ( $F_n$ ) and tangential ( $F_t$ ) components of the cutting force occur. Experiments based on the method of scratching [37, 38], aimed to establish the relationship between the range of plastic deformation depending on the processing parameters, i.e., the relationship between the ductile mode and cutting speed.

All these researches have a similar goal, and that is to find and describe precise mechanisms that explain the phenomena created in the process of micro-cutting of brittle materials. S. Malkin and T.W. Hwang [39].

In the micro-cutting mechanism itself, a very important influencing factor is the depth of cut, and the influence of elastic deformations of the material. The depth of cut is in direct correlation with the cutting mode (ductile or brittle fracture mode) in which the micro-cutting process takes place. This has the consequence that the amount of material removed in the process of micro-cutting of brittle materials is a direct function of the depth of tool penetration. G. Subhash et al. [40] tried to find a method that can be used to determine the mode in which processing is currently performed. The research was based on the analysis of the values of forces that occur during micro-cutting using the "data dependent system (DDS)" method. The main goal was to determine which of the two modes is currently being processed, depending on the intensity and character of the cutting force.

A clearer picture of crack formation and shear planes during the micro-cutting process was examined by D. Ghost et al. [41] using a combined "Boussinesq" and "Cerruti - field solution" method. The experiments were performed on Zirconium Diboride-Silicon Carbide composite material. In addition to these studies, R. Anton [42] and D. Ghost [43] conducted a similar analysis, but on a different material, with the aim of determining the change in mechanical properties of the material during indentation under static and dynamic force.

Researchers [44-48] based their experiments on the development of a mathematical model of micro-cutting of brittle materials. By implementing these algorithms in software packages, which deal with finite element methods, the possibility of predicting the phenomena that occur during the micro-cutting process is realized.

### ***Examination of the influence of the kinematics of the micro-cutting process on the machinability of brittle materials***

In the 1950s of the last century, research on the influence of tool trajectory on the machinability of materials began [49, 50]. However, expansion in this area began only in the 1990s when T. Moriwaki et al [51, 52] conducted a micro-cutting experiment with oscillatory tool movement. It was then determined that in relation to conventional cutting of brittle materials, where the tool performs a relatively rectilinear movement in relation to the workpiece, the range of ductile mode can be increased by applying vibratory (oscillatory) movement of the tool. This has also been confirmed in

research [53-55]. This type of micro-cutting leads to a decrease in the intensity of forces that occur during the machining process, as shown by M. Zhou et al. [56].

V.K. Astashev and V.I. Babitsky [57] came up with a mathematical model that arrives at the value of the cutting force intensity as a function of the vibrational micro-cutting parameters.

Micro cutting, in which the tool achieves a complex oscillatory movement, requires a special tool geometry in order to achieve the desired movement. Among the first to develop such a system were L. Hahn and co-workers [58]. Their system is specific in that it has the possibility of error compensation. However, one of the problems that occurs with this type of micro-cutting is keeping the tool in a resonant state if there is a change in the intensity of the cutting forces. V. I. Babitsky et al [59] developed a mechatronic system by which the tool is maintained in a resonant state regardless of the change in the value of the cutting force intensity.

Although the oscillatory movement of the tool increases its lifespan, due to the intense friction between the flank surface of the tool and the machined surface of the workpiece, more intensive wear of the flank surface occurs. By changing the direction of oscillation of the tool, which avoids contact of the tool with the workpiece in the return, and to a large extent in the working stroke, there is an additional increase in tool lifespan, as shown by M. Jin and M. Murakawa [60].

T. Moriwaki and E. Shamoto [61-63] conducted an upgraded vibration cutting experiment, the so-called elliptical vibration cutting. For the purposes of this type of experiment, where the tool achieves vibrational elliptical motion, a special tool system was developed and presented by E. Shamoto [64]. In order to obtain greater flexibility during the performance of experiments, the developed system had the possibility of independently defining the oscillation amplitudes in two directions, which achieves the desired orientation of the tool oscillation. This type of micro-cutting has determined that the service life of the tool increases in relation to the rectilinear vibratory micro-cutting. Also, during machining of grooves in brittle materials with elliptical movement of the tool, a better geometry of the groove is achieved in relation to the processing where the tool performs a rectilinear oscillatory movement [65].

Processing of materials with pronounced plastic properties is characterized by obtaining a better-quality surface [66]. N. Suzuki and co-workers [67] by applying the elliptical movement of the tool managed to realize the processing of molds for casting lenses made of Wolfram alloys, which was not feasible until that moment. On the other hand, C. Ma et al [68] found that scraping achieves better machining accuracy compared to conventional scraping, even when the tool achieves rectilinear oscillatory motion. In addition, this eliminates the possibility of cracking at the edges of the workpiece [69].

The values of the force intensities that occur in the contact of the tool that achieves the oscillatory elliptical motion and the workpiece are reduced in comparison with the values of the force intensities in the conventional movement of the tool. Models for precise prediction of force intensity have been presented by both N. Negishi [70] and C. Ma [68, 69].

N. Suzuki and co-workers [71] developed a system for controlling the depth of cut with the help of oscillation amplitude variation. This method has increased the efficiency of such a system. The development of similar systems can be found in other researchers [72, 73].

#### ***Examination of the influence of tool geometry on the micro-cutting process***

In addition to examining the effect of forces during the process of indentation/micro-cutting, as well as the process of material separation, research has focused on examining the influence of tool or indenter geometry on the process of micro-cutting/material separation. Unlike macro-cutting, where the depth of cut is significantly greater than the value of the tool tip radius, and therefore its impact can be neglected, this is not the case with micro-cutting. The rounding of the tool tip is a very influential factor that affects the micro-cutting process itself, bearing in mind that the value of its radius is greater than the value of the depth at which the tool penetrates the material. As a consequence, the value of the rake angle of the tool changes, which is a function of the depth of cut and the value of the tool tip radius. The change in the value of the rake angle has a direct impact on the increase or decrease of compressive stresses in the cutting zone, as a result of which the process of chip formation can differ in different zones of cutting depth.

Examining the influence of tool geometry on the micro-cutting process has been far more investigated on materials with pronounced plastic properties, compared to materials that are brittle in nature.

Z.J. Yuan [74] examined in detail the influence of the tool tip radius value on the critical penetration depth for a material with pronounced plastic properties. He primarily based his research on the observation of the dependence of the critical depth that leads to the formation of chip in the form of extrusion from the value of the tool tip radius. It turned out that a tool with a smaller value of the tool tip radius leads to a reduction of the limit below which there is no separation of material. Below the critical values of the depth of micro-cutting, the material is elastically and plastically deformed. This can be explained by the change in the effective value of the rake angle proved by Z. Fang in his work [75]. His research has shown that the effective value of the rake angle, which is a function of the value of the depth of cut and the tool tip radius, has a significant influence on the direction of propagation of the stress field within the material. Many subsequent studies have been conducted on a similar topic [76-82].

Changing the geometry of the tool tip, i.e., the value of the tool tip radius, can have a great impact on the intensities of forces that occur during the machining process, and thus a direct impact on tool wear during the machining process [83]. With this in mind, part of the research in the field of micro-cutting is focused on the development of a mathematical model for the prediction of forces arising in the cutting zone. One such study is that conducted by G. Bissacco et al. [84] whose presented model took into account the value of the tool tip radius. On the other hand, research conducted by M. Malekian et al. [85], formed a model of force prediction in which, in addition to the value of the tool tip radius, the influence of elastic return of material is incorporated. Research related to the formation of force prediction models in micro-cutting using the finite element method can also be found in the literature [86].

The geometry of the tool tip can also have a significant effect on the geometry of the machined surface. If we are talking about grooving by the method of scratching, different tool geometries lead to a change in the geometry of the

formed groove. One such study was conducted by D. Axinte et al. [87] On the other hand, the value of the tool tip radius can have a great influence on the size of the burrs that are formed on the edges of the surface. Decreasing the value of the ratio of the depth of micro-cutting and the value of the tool tip radius, leads to an increase in the value of the raised edge along the trace of micro-cuts [88, 89].

#### ***Micro cutting of stone-based materials***

Stone-based materials such as granite or marble are difficult to process. Their pronounced brittleness and high hardness, which is also variable within the entire volume, have a great influence on the processing of these materials. The variability of the hardness values of these materials leads to the complexity of choosing the optimal machining parameters, such as depth and cutting speed, which results in machining inefficiencies in the domain of tool consumption and obtaining the desired surface quality. If we take into account the increasing use of stone-based materials, as well as their huge potential for wider application, more intensive research in the field of machinability of these materials becomes justified.

As already mentioned, the main goal in micro-cutting of brittle materials is to obtain a finely machined surface without the presence of traces of material destruction. H. Huang et al [90] found in their research that granite, although brittle in nature, can be processed in a ductile mode, thus obtaining a high-gloss surface. Also, they came to the conclusion that with the increase of plastic deformations in the cutting zone, the roughness of the machined surface decreases. In their research, similar conclusions were reached by the authors [91].

Although there is a large variation in hardness within the entire volume of granite due to its heterogeneous composition, the hardness can additionally differ between different types (varieties) of granite, due to the different minerals from which they are formed. Research has shown that different material properties, such as hardness, can affect the range of ductile mode [76, 92-94]. A model that would take this into account, and which would serve to determine the optimal processing parameters based on the value and variation of the hardness of the material, was presented by J. Xie and J. Tamaki [95]. They came to it on the basis of experiments conducted on ten different types of granite. On the other hand, Y. Li et al. [96] presented a new method of granite processing that increases the durability of tools by having a specially designed tool geometry to influence the friction that occurs during tool-workpiece interactions.

Marble, in addition to granite, is one of the most present stone-based materials with increasing application in industry. Similar to granite, by its nature, marble is a very brittle material with a heterogeneous structure. Depending on the type of minerals that are part of marble, its hardness can vary significantly. In previous research, marble, like most other brittle materials, can be processed in both the brittle fracture mode and the ductile mode [97], however, a small number of studies on this topic have been published so far.

#### ***References:***

1. Merchant, M. Eugene. "Mechanics of the metal cutting process. I. Orthogonal cutting and a type 2 chip." *Journal of applied physics* 16.5 (1945): 267-275.
2. Merchant, M. Eugene. "Mechanics of the metal cutting process. II. Plasticity conditions in orthogonal cutting." *Journal of applied physics* 16.6 (1945): 318-324.
3. Guzel, B. U., and I. Lazoglu. "Increasing productivity in sculpture surface machining via off-line piecewise variable feedrate scheduling based on the force system model." *International Journal of Machine Tools and Manufacture* 44.1 (2004): 21-28.
4. Ip, Ralph WL, Henry CW Lau, and Felix TS Chan. "An economical sculptured surface machining approach using fuzzy models and ball-nosed cutters." *Journal of Materials Processing Technology* 138.1-3 (2003): 579-585.
5. Li, Z. Z., et al. "A solid model-based milling process simulation and optimization system integrated with CAD/CAM." *Journal of Materials Processing Technology* 138.1-3 (2003): 513-517.
6. Wang, Wen Ping. "Solid modeling for optimizing metal removal of three-dimensional NC end milling." *Journal of Manufacturing Systems* 7.1 (1988): 57-65.
7. Yazar, Zeki, et al. "Feed rate optimization based on cutting force calculations in 3-axis milling of dies and molds with sculptured surfaces." *International Journal of Machine Tools and Manufacture* 34.3 (1994): 365-377.
8. Tanović. Lj. "Current investigation in the field of micro-grinding." *Proceedings of the XIV International Conference Maintenance And Production Engineering "KODIP-2014"*, Engineering Academy of Montenegro (2014): 29-35.
9. Liu, K., X. P. Li, and M. Rahman. "Characteristics of high speed micro-cutting of tungsten carbide." *Journal of Materials Processing Technology* 140.1-3 (2003): 352-357.
10. Kim, Jeong-Du, and In-Hyu Choi. "Micro surface phenomenon of ductile cutting in the ultrasonic vibration cutting of optical plastics." *Journal of materials processing technology* 68.1 (1997): 89-98.
11. Nakasuji, T., et al. "Diamond turning of brittle materials for optical components." *CIRP annals* 39.1 (1990): 89-92.
12. Yan, Jiwang, Katsuo Syoji, and Jun'ichi Tamaki. "Some observations on the wear of diamond tools in ultra-precision cutting of single-crystal silicon." *Wear* 255.7-12 (2003): 1380-1387.
13. Arif, Muhammad, Mustafizur Rahman, and Wong Yoke San. "Ultraprecision ductile mode machining of glass by micromilling process." *Journal of Manufacturing Processes* 13.1 (2011): 50-59.
14. Simoneau, A., E. Ng, and M. A. Elbestawi. "Chip formation during microscale cutting of a medium carbon steel." *International Journal of Machine Tools and Manufacture* 46.5 (2006): 467-481.
15. Simoneau, A., E. Ng, and M. A. Elbestawi. "The effect of microstructure on chip formation and surface defects in microscale, mesoscale, and macroscale cutting of steel." *CIRP annals* 55.1 (2006): 97-102.
16. Simoneau, A., Elbestawi Ng, and M. A. Elbestawi. "Surface defects during microcutting." *International Journal of Machine Tools and Manufacture* 46.12-13 (2006): 1378-1387.

17. Liu, Kai, and Shreyes N. Melkote. "Finite element analysis of the influence of tool edge radius on size effect in orthogonal micro-cutting process." *International Journal of Mechanical Sciences* 49.5 (2007): 650-660.
18. Simoneau, A., E. Ng, and M. A. Elbestawi. "Grain size and orientation effects when microcutting AISI 1045 steel." *CIRP annals* 56.1 (2007): 57-60.
19. Subbiah, Sathyan, and Shreyes N. Melkote. "Effect of finite edge radius on ductile fracture ahead of the cutting tool edge in micro-cutting of Al2024-T3." *Materials Science and Engineering: A* 474.1-2 (2008): 283-300.
20. Woon, K. S., et al. "Investigations of tool edge radius effect in micromachining: a FEM simulation approach." *Journal of materials processing technology* 195.1-3 (2008): 204-211.
21. Zhou, Jun, et al. "The influence of tool edge radius on size effect in orthogonal micro-cutting process of 7050-t7451 aluminum alloy." *Key Engineering Materials*. Vol. 375. Trans Tech Publications Ltd, 2008.
22. Ducobu, F., E. Filippi, and E. Rivière-Lorphèvre. "Chip formation and minimum chip thickness in micro-milling." *Proceedings of the 12th CIRP conference on modeling of machining operations*. Vol. 1. 2009.
23. Woon, K. S., and M. Rahman. "Extrusion-like chip formation mechanism and its role in suppressing void nucleation." *CIRP annals* 59.1 (2010): 129-132.
24. Zhanqiang, Liu, Shi Zhenyu, and Wan Yi. "Definition and determination of the minimum uncut chip thickness of microcutting." *The International Journal of Advanced Manufacturing Technology* 69.5 (2013): 1219-1232.
25. Lawn, Brian, and Rodney Wilshaw. "Indentation fracture: principles and applications." *Journal of materials science* 10.6 (1975): 1049-1081.
26. Evans, A. G., and To R. Wilshaw. "Quasi-static solid particle damage in brittle solids—I. Observations analysis and implications." *Acta Metallurgica* 24.10 (1976): 939-956.
27. Lawn, B. R., and A. G. Evans. "A model for crack initiation in elastic/plastic indentation fields." *Journal of Materials Science* 12.11 (1977): 2195-2199.
28. Marshall, D. B., and Brian R. Lawn. "Residual stress effects in sharp contact cracking: Part 1: Indentation fracture mechanics." *Journal of Materials Science* 14.8 (1979): 2001-2012.
29. Marshall, D. B., Brian R. Lawn and P. Chantikul. "Residual stress effects in sharp contact cracking: Part 2: Strength degradation." *Journal of Materials Science* 14.8 (1979): 2225-2235.
30. Lawn, B. Ro, and M. V. Swain. "Microfracture beneath point indentations in brittle solids." *Journal of materials science* 10.1 (1975): 113-122.
31. Marshall, D. B., B. R. Lawn, and A. G. Evans. "Elastic/plastic indentation damage in ceramics: the lateral crack system." *Journal of the American Ceramic Society* 65.11 (1982): 561-566.
32. Lawn, B. Ro, and E. Ro Fuller. "Equilibrium penny-like cracks in indentation fracture." *Journal of Materials Science* 10.12 (1975): 2016-2024.
33. Lawn, Brian R., A. G. Evans, and D. B. Marshall. "Elastic/plastic indentation damage in ceramics: the median/radial crack system." *Journal of the American Ceramic Society* 63.9-10 (1980): 574-581.
34. Marshall, David B. "Controlled flaws in ceramics: a comparison of Knoop and Vickers indentation." *Journal of the American Ceramic Society* 66.2 (1983): 127-131.
35. Marshall, David B. "Geometrical effects in elastic/plastic indentation." *Journal of the American Ceramic Society* 67.1 (1984): 57-60.
36. Chandra, A., et al. "Role of unloading in machining of brittle materials." *J. Manuf. Sci. Eng.* 122.3 (2000): 452-462.
37. Stojadinovic, Slavenko, Ljubodrag Tanovic, and Sreten Savicevic. "Micro-cutting mechanisms in silicon nitride ceramics Silinit R grinding." *中國機械工程學刊* 36.4 (2015): 291-297.
38. Mladenovic, G., et al. "Experimental investigation of microcutting mechanisms in oxide ceramic CM332 grinding." *Journal of Manufacturing Science and Engineering* 137.3 (2015).
39. Malkin, S., and T. W. Hwang. "Grinding mechanisms for ceramics." *CIRP annals* 45.2 (1996): 569-580.
40. Subhash, Ghatu, Josh E. Loukus, and Sudhakar M. Pandit. "Application of data dependent systems approach for evaluation of fracture modes during a single-grit scratching." *Mechanics of materials* 34.1 (2002): 25-42.
41. Ghosh, Dipankar, et al. "Scratch-induced microplasticity and microcracking in zirconium diboride-silicon carbide composite." *Acta Materialia* 56.13 (2008): 3011-3022.
42. Anton, Richard J., and Ghatu Subhash. "Dynamic Vickers indentation of brittle materials." *Wear* 239.1 (2000): 27-35.
43. Ghosh, Dipankar, et al. "Dynamic indentation response of fine-grained boron carbide." *Journal of the American Ceramic Society* 90.6 (2007): 1850-1857.
44. Ueda, K., et al. "A J-integral approach to material removal mechanisms in microcutting of ceramics." *CIRP annals* 40.1 (1991): 61-64.
45. Inamura, Toyoshiro, et al. "Brittle/ductile transition phenomena observed in computer simulations of machining defect-free monocrystalline silicon." *CIRP Annals* 46.1 (1997): 31-34.
46. Subbiah, Sathyan, and Shreyes N. Melkote. "Evidence of ductile tearing ahead of the cutting tool and modeling the energy consumed in material separation in micro-cutting." (2007): 321-331.
47. Chiaia, Bernardino. "Fracture mechanisms induced in a brittle material by a hard cutting indenter." *International Journal of Solids and structures* 38.44-45 (2001): 7747-7768.
48. Tan, Yuanqiang, Dongmin Yang, and Yong Sheng. "Study of polycrystalline Al2O3 machining cracks using discrete element method." *International Journal of Machine Tools and Manufacture* 48.9 (2008): 975-982.
49. Colwell, L. V. "The effects of high-frequency vibrations in grinding." *Trans. ASME* 78.4 (1956): 837.

50. Dohmen, Hans-Gerd. Zerspanungsuntersuchungen beim drehen mit periodisch bewegtem schneidwerkzeug. Diss. Rheinisch-Westfälische Technische Hochschule Aachen, 1964.
51. Moriwaki, Toshimichi, and Eiji Shamoto. "Ultraprecision diamond turning of stainless steel by applying ultrasonic vibration." *CIRP annals* 40.1 (1991): 559.
52. Moriwaki, Toshimichi, Eiji Shamoto, and Kenji Inoue. "Ultraprecision ductile cutting of glass by applying ultrasonic vibration." *CIRP annals* 41.1 (1992).
53. Zhou, Ming, et al. "Brittle-ductile transition in the diamond cutting of glasses with the aid of ultrasonic vibration." *Journal of Materials Processing Technology* 121.2-3 (2002): 243-251.
54. Gan, J., et al. "Ultraprecision diamond turning of glass with ultrasonic vibration." *The International Journal of Advanced Manufacturing Technology* 21.12 (2003): 952-955.
55. Liu, K., et al. "Study of ductile mode cutting in grooving of tungsten carbide with and without ultrasonic vibration assistance." *The International Journal of Advanced Manufacturing Technology* 24.5 (2004): 389-394.
56. Zhou, Ming, et al. "Vibration-assisted precision machining of steel with PCD tools." *Materials and manufacturing processes* 18.5 (2003): 825-834.
57. Astashev, V. K., and V. I. Babitsky. "Ultrasonic cutting as a nonlinear (vibro-impact) process." *Ultrasonics* 36.1-5 (1998): 89-96.
58. Han, Liang, Weiliang Xu, and Shiu Kit Tso. "Ultrasonically assisted and piezoelectric actuators integrated cutting tool." *Japanese journal of applied physics* 37.8R (1998): 4616.
59. Babitsky, V. I., A. N. Kalashnikov, and F. V. Molodtsov. "Autoresonant control of ultrasonically assisted cutting." *Mechatronics* 14.1 (2004): 91-114.
60. Jin, Masahiko, and Masao Murakawa. "Development of a practical ultrasonic vibration cutting tool system." *Journal of materials processing technology* 113.1-3 (2001): 342-347.
61. Shamoto, Eiji, and Toshimichi Moriwaki. "Study on elliptical vibration cutting." *CIRP annals* 43.1 (1994): 35-38.
62. Moriwaki, Toshimichi, and Eiji Shamoto. "Ultrasonic elliptical vibration cutting." *CIRP annals* 44.1 (1995): 31-34.
63. Shamoto, Eiji, and Toshimichi Moriwaki. "Ultraprecision diamond cutting of hardened steel by applying elliptical vibration cutting." *CIRP Annals* 48.1 (1999): 441-444.
64. Shamoto, Eiji, et al. "Development of ultrasonic elliptical vibration controller for elliptical vibration cutting." *CIRP Annals* 51.1 (2002): 327-330.
65. Lee, Jun-Seok, et al. "A study on micro-grooving characteristics of planar lightwave circuit and glass using ultrasonic vibration cutting." *Journal of materials processing technology* 130 (2002): 396-400.
66. Ahn, Jung-Hwan, Han-Seok Lim, and Seong-Min Son. "Improvement of micro-machining accuracy by 2-dimensional vibration cutting." *Proc ASPE*. Vol. 20. 1999.
67. Suzuki, N., et al. "Elliptical vibration cutting of tungsten alloy molds for optical glass parts." *CIRP annals* 56.1 (2007): 127-130.
68. Ma, Chunxiang, et al. "Study of machining accuracy in ultrasonic elliptical vibration cutting." *International Journal of Machine Tools and Manufacture* 44.12-13 (2004): 1305-1310.
69. Ma, Chunxiang, et al. "Suppression of burrs in turning with ultrasonic elliptical vibration cutting." *International Journal of Machine Tools and Manufacture* 45.11 (2005): 1295-1300.
70. Negishi, Nobuhiko. "Elliptical vibration assisted machining with single crystal diamond tools." (2003).
71. Suzuki, Norikazu, Hideo Yokoi, and Eiji Shamoto. "Micro/nano sculpturing of hardened steel by controlling vibration amplitude in elliptical vibration cutting." *Precision Engineering* 35.1 (2011): 44-50.
72. Overcash, J. "Development of a tunable ultrasonic vibration-assisted diamond turning instrument." *Proc ASPE*. Vol. 30. 2003.
73. Li, Xun, and Deyuan Zhang. "Ultrasonic elliptical vibration transducer driven by single actuator and its application in precision cutting." *Journal of materials processing technology* 180.1-3 (2006): 91-95.
74. Yuan, Z. J., M. Zhou, and S. Dong. "Effect of diamond tool sharpness on minimum cutting thickness and cutting surface integrity in ultraprecision machining." *Journal of Materials Processing Technology* 62.4 (1996): 327-330.
75. Fang, F. Z., H. Wu, and Y. C. Liu. "Modelling and experimental investigation on nanometric cutting of monocrystalline silicon." *International Journal of Machine Tools and Manufacture* 45.15 (2005): 1681-1686.
76. Son, Seong Min, Han Seok Lim, and Jung Hwan Ahn. "Effects of the friction coefficient on the minimum cutting thickness in micro cutting." *International Journal of Machine Tools and Manufacture* 45.4-5 (2005): 529-535.
77. Lai, Xinmin, et al. "Modelling and analysis of micro scale milling considering size effect, micro cutter edge radius and minimum chip thickness." *International Journal of Machine Tools and Manufacture* 48.1 (2008): 1-14.
78. Bissacco, Giuliano, Hans Nørgaard Hansen, and Leonardo De Chiffre. "Micromilling of hardened tool steel for mould making applications." *Journal of Materials Processing Technology* 167.2-3 (2005): 201-207.
79. Aramcharoen, A., and P. T. Mativenga. "Size effect and tool geometry in micromilling of tool steel." *Precision Engineering* 33.4 (2009): 402-407.
80. Özel, T., X. Liu, and A. Dhanorker. "Modelling and simulation of micro-milling process." 4th International Conference and Exhibition on Design and Production of Machines and Dies/Molds. 2007.
81. Lee, Kiha, and David A. Dornfeld. "Micro-burr formation and minimization through process control." *Precision Engineering* 29.2 (2005): 246-252.
82. Woon, K. S., et al. "The effect of tool edge radius on the contact phenomenon of tool-based micromachining." *International Journal of Machine Tools and Manufacture* 48.12-13 (2008): 1395-1407.

83. Elkaseer, A. M., et al. "Material microstructure effect-based investigation of tool wear in micro-endmilling of multi-phase materials." Proceedings of the 7th International Conference on Multi-Material Micro Manufacture, Bourg en Bresse and Oyonnax, France. 2010.
84. Bissacco, Giuliano, Hans Nørgaard Hansen, and J. Slunsky. "Modelling the cutting edge radius size effect for force prediction in micro milling." CIRP annals 57.1 (2008): 113-116.
85. Malekian, Mohammad, Simon S. Park, and Martin BG Jun. "Modeling of dynamic micro-milling cutting forces." International Journal of Machine Tools and Manufacture 49.7-8 (2009): 586-598.
86. Afazov, S. M., S. M. Ratchev, and J. Segal. "Modelling and simulation of micro-milling cutting forces." Journal of Materials Processing Technology 210.15 (2010): 2154-2162.
87. Axinte, D., et al. "On the influence of single grit micro-geometry on grinding behavior of ductile and brittle materials." International Journal of Machine Tools and Manufacture 74 (2013): 12-18.
88. Fang, F. Z., and Y. C. Liu. "On minimum exit-burr in micro cutting." Journal of Micromechanics and Microengineering 14.7 (2004): 984.
89. Zhang, Tao, Zhanqiang Liu, and Chonghai Xu. "Influence of size effect on burr formation in micro cutting." The International Journal of Advanced Manufacturing Technology 68.9 (2013): 1911-1917.
90. Huang, H., et al. "Micro-structure detection of a glossy granite surface machined by the grinding process." Journal of materials processing technology 129.1-3 (2002): 403-407.
91. Tanovic, Lj, et al. "Experimental investigation of microcutting mechanisms in granite grinding." Journal of manufacturing science and engineering 133.2 (2011).
92. Kim, Chang-Ju, J. Rhett Mayor, and Jun Ni. "A static model of chip formation in microscale milling." J. Manuf. Sci. Eng. 126.4 (2004): 710-718.
93. Weule, H., V. Hüntrup, and H. Tritschler. "Micro-cutting of steel to meet new requirements in miniaturization." CIRP Annals 50.1 (2001): 61-64.
94. Vogler, Michael P., Richard E. DeVor, and Shiv G. Kapoor. "On the modeling and analysis of machining performance in micro-endmilling, part I: surface generation." J. Manuf. Sci. Eng. 126.4 (2004): 685-694.
95. Xie, J., and J. Tamaki. "Parameterization of micro-hardness distribution in granite related to abrasive machining performance." Journal of Materials Processing Technology 186.1-3 (2007): 253-258.
96. Li, Yuan, et al. "Cost-effective machining of granite by reducing tribological interactions." Journal of materials processing technology 129.1-3 (2002): 389-394.
97. Tanovic, L. J., et al. "Experimental investigation of microcutting mechanisms in marble grinding." Journal of manufacturing science and engineering 131.6 (2009).